Discrete empirical interpolation in POD Model
Order Reduction of Drift-Diffusion Equations in Electrical Networks

M. Hinze, and M. Kunkel
Discrete empirical interpolation in POD Model Order Reduction of Drift-Diffusion Equations in Electrical Networks

Michael Hinze and Martin Kunkel

Abstract We consider model order reduction of integrated circuits with semiconductors modeled by modified nodal analysis and drift-diffusion (DD) equations. The DD-equations are discretized in space using a mixed finite element method. This discretization yields a high dimensional, nonlinear system of differential-algebraic equations. Proper orthogonal decomposition (POD) is used to reduce the dimension of this model. Since the computational complexity of the reduced model through the nonlinearity of the DD equations still depends on the number of variables of the full model we apply the Discrete Empirical Interpolation Method (DEIM) to further reduce the computational complexity. We provide numerical comparisons which demonstrate the performance of this approach.

1 Introduction

In this article we investigate POD-based model order reduction for semiconductors in electrical networks using DEIM to treat the reduction of nonlinear components. Electrical networks can be modeled efficiently by a differential-algebraic equation (DAE) which is obtained from modified nodal analysis. Often semiconductors themselves are modeled by electrical networks. These models are stored in a library and are stamped into the surrounding network in order to create a complete model of the integrated circuit. In [4] POD model order reduction (POD-MOR) is proposed to obtain a reduced surrogate model conserving as much of the DD structure as possible in the reduced order model. This approach in [5] is extended to parametrized
electrical networks using the greedy sampling proposed in [6]. Advantages of the 
POD approach are the higher accuracy of the model and fewer model parameters. 
On the other hand, numerical simulations are more expensive. For a comprehensive 
overview of the drift-diffusion equations we refer to [1–3].

Using the Notation introduced in [7, 8] the finite element discretization of one 
semiconductor with domain $\Omega \subset \mathbb{R}^d$ ($d=1,2,3$) in an electrical network leads to a 
nonlinear, fully coupled DAE system of the form

\[
\begin{align*}
A_C \frac{d}{dt} q_C(A_C e(t), t) + A_R g(A_R e(t), t) + A_L j_L(t) + A_V j_V(t) + A_{\psi} j_{\psi}(t) &= 0, \\
\frac{d}{dt} \phi_L(j_L(t), t) - A_L e(t) &= 0, \\
A_V e(t) - \nu_{\psi}(t) &= 0, \\
q_S(t) - \frac{d g_{\psi}(t)}{dt} &= 0, \\
j_S(t) - C_1 J_n(t) - C_2 J_p(t) - C_3 q_S(t) &= 0,
\end{align*}
\]

compare Fig. 1, and see [4, 5]. Here, (1)-(3) describe the electrical network with 
unknown node potentials $e$, and branch currents $j_L$ of inductive, and $j_V$ of voltage 
source branches, respectively. Equations (4)-(5) are discretized coupling conditions.
The vector-valued function $\psi$ contains the weights for the ansatz functions $\phi_i$ in the 
Galerkin ansatz

\[
\psi^h(t,x) = \sum_{i=1}^{N} \psi(t) \phi_i(x), \quad x \in \Omega,
\]

for the discretized potential of the semiconductor. $N$ denotes the number of finite 
elements. The discretized electron and hole concentrations $n^h_i(t, x)$ and $p^h_i(t, x)$, the 
electric field $-g^h_{\psi}(t, x)$ and the current densities $J^h_n(t, x)$ and $J^h_p(t, x)$ are defined likewise. The incidence matrix $A = [A_R, A_C, A_L, A_V, A_{\psi}, A_{\psi}]$ represents the network topology and is defined as usual. The matrices $A_{FEM}$ and $M_L$ are large and sparse. The 
voltage sources $v_i$ and current sources $i_j$ are considered as inputs of the network.

This paper is organized as follows. In Sect. 2 we present the model order reduction 
method based on snapshot POD combined with DEIM. In Sect. 3 we present 
numerical experiments, and also discuss advantages and shortcomings of our approach.
Fig. 1 Basic test circuit with one diode. The network is described by
\[ A_V = (1, 0)^\top, \]
\[ A_S = (-1, 1)^\top, \]
\[ A_R = (0, 1)^\top, \]
\[ g(A_R e, t) = \frac{1}{R} e_2(t). \]

2 Model order reduction

We use POD-MOR applied to the DD part (6) to construct a dimension-reduced surrogate model for (1)-(6). For this purpose we run a simulation of the unreduced system and collect snapshots \( \psi(t_k, \cdot), n(t_k, \cdot), p(t_k, \cdot), g(t_k, \cdot), J(t_k, \cdot) \) at time instances \( t_k \in \{t_1, \ldots, t_l\} \subset [0, T] \). The optimal selection of the time instances is not considered here. We use the time instances delivered by the DAE integrator. The snapshot variant of POD introduced in [9] finds a best approximation of the space spanned by the snapshots w.r.t. to the considered scalar product.

Since every component of the state vector \( z := (\psi, n, p, g, J_n, J_p) \) has its own physical meaning we apply POD MOR to each component separately. Among other things this approach has the advantage of yielding a block-dense model and the approximation quality of each component is adapted individually.

The time-snapshot POD procedure delivers Galerkin ansatz spaces for \( \psi, n, p, g, J_n, J_p \) and we set \( \psi_{\text{POD}}(t) := U_{\psi} \gamma_{\psi}(t), n_{\text{POD}}(t) := U_n \gamma_n(t), \ldots \). The injection matrices \( U_{\psi} \in \mathbb{R}^{N \times s_{\psi}}, U_n \in \mathbb{R}^{N \times s_n}, \ldots \), contain the (time independent) POD basis functions, and the vectors \( \gamma(\cdot) \) the corresponding time-variant coefficients. The numbers \( s(\cdot) \) denote the respective number of POD basis functions included. Assembling the POD system yields the reduced model

\[ A_C \frac{d}{dt} q_C(A_C e(t), t) + A_{\psi} g(A_R e(t), t) + A_L j_L(t) + A_V j_V(t) + A_S j_S(t) + A_{IS} s(t) = 0, \quad (8) \]

\[ A_{\psi} j_L(t, t) - A_L e(t) = 0, \quad (9) \]

\[ A_{\psi} e(t) - \psi_L(t) = 0, \quad (10) \]

\[ q(t) - U_{\psi} \frac{dg}{dt}(t) = 0, \quad (11) \]

\[ j(t) - C_1 U_{\psi} \gamma_{\psi}(t) - C_2 U_{\psi} \gamma_{p}(t) - C_3 q_{\psi}(t) = 0, \quad (12) \]
\[\begin{pmatrix}
\frac{\partial \gamma_p}{\partial t}(t) \\
\frac{\partial \gamma_d}{\partial t}(t) \\
0 \\
0
\end{pmatrix} + A_{POD} \begin{pmatrix}
\gamma_p(t) \\
\gamma_d(t) \\
\gamma_{\psi_p}(t) \\
\gamma_{\psi_d}(t)
\end{pmatrix} + U^T F(U_n \gamma_n(t), U_p \gamma_p(t), U_{\psi_n} \gamma_{\psi_n}(t), U_{\psi_p} \gamma_{\psi_p}(t))
\]

\[-U^T b(e(t)) = 0, \quad (13)\]

with \(A_{POD} = U^T A_{FEM} U\) and \(U = \text{diag}(U_\psi, U_n, U_p, U_{\psi_n}, U_{\psi_p}, U_{\psi_d})\). All matrix-matrix multiplications are calculated in an offline-phase. The nonlinear function \(F\) has to be evaluated online which means that the computational complexity of the reduced order model still depends on the number of unknowns of the unreduced model. The nonlinearity in (13) is given by

\[
U^T F(U \gamma(t)) = \begin{pmatrix}
0 \\
U^T_{n} F_n(U_n \gamma_n(t), U_p \gamma_p(t)) \\
U^T_{p} F_p(U_n \gamma_n(t), U_p \gamma_p(t)) \\
0 \\
U^T_{p} F_p(U_n \gamma_n(t), U_p \gamma_p(t)) \\
U^T_{p} F_p(U_n \gamma_n(t), U_p \gamma_p(t))
\end{pmatrix},
\]

see e.g. [5]. The subsequent considerations apply for each block component of \(F\). For the sake of presentation we only consider the second block

\[
\begin{pmatrix}
U_n^T \\
\text{size } s_n \times N
\end{pmatrix}
\begin{pmatrix}
F_n \\
\text{size } N \times s_n
\end{pmatrix}
\begin{pmatrix}
\gamma_n(t) \\
\gamma_p(t)
\end{pmatrix},
\quad (14)
\]

and its derivative with respect to \(\gamma_p\),

\[
\begin{pmatrix}
U_n^T \\
\text{size } s_n \times N
\end{pmatrix}
\begin{pmatrix}
\frac{\partial F_n}{\partial p} (U_n \gamma_n(t), U_p \gamma_p(t)) \\
\text{size } N \times N, \text{ sparse}
\end{pmatrix}
\begin{pmatrix}
\gamma_n(t) \\
\gamma_p(t)
\end{pmatrix}.
\]

Here, the matrices \(U_i\), are dense and the Jacobian of \(F_n\) is sparse. The evaluation of (14) is of computational complexity \(O(N)\). Furthermore, we need to multiply large dense matrices in the evaluation of the Jacobian. Thus, the POD model order reduction may become inefficient.

To overcome this problem, we apply Discrete Empirical Interpolation Method (DEIM) proposed in [10], which we now describe briefly. The snapshots \(\psi^h(t_k, \cdot), \quad n^h(t_k, \cdot), \quad p^h(t_k, \cdot), \quad \gamma^h_{\psi_p}(t_k, \cdot), \quad \gamma^h_{\psi_d}(t_k, \cdot)\) are collected at time instances \(t_k \in \{t_1, \ldots, t_L\} \subset [0, T]\) as before. Additionally, we collect snapshots \(\{F_n(n(t_k), p(t_k))\}\) of the nonlinearity. DEIM approximates the projected function (14) such that

\[
U_n^T F_n(U_n \gamma_n(t), U_p \gamma_p(t)) \approx (U_n^T F_n (P_n^T P_n)^{-1}) P_n^T F_n(U_n \gamma_n(t), U_p \gamma_p(t),)
\]
where $V_\tau \in \mathbb{R}^{N \times \tau_\tau}$ contains the first $\tau_\tau$ POD basis functions of the space spanned by the snapshots $\{F_n(n(t_k),p(t_k))\}$ associated with the largest singular values. The selection matrix $P_\tau = (e_{\rho_1}, \ldots, e_{\rho_\tau}) \in \mathbb{R}^{N \times \tau_\tau}$ selects the rows of $F_n$ corresponding to the so-called DEIM indices $\rho_1, \ldots, \rho_\tau$, which are chosen such that the growth of a global error bound is limited and $P_\tau^T V_\tau$ is regular, see [10] for details.

The matrix $W_\tau := (U_\tau^T V_\tau (P_\tau^T V_\tau)^{-1}) \in \mathbb{R}^{\tau_\tau \times \tau_\tau}$ as well as the whole interpolation method is calculated in an offline phase. In the simulation of the reduced order model we instead of (14) evaluate:

$$W_\tau \quad \text{size } \tau_\tau \times \tau_\tau \quad P_\tau^T V_\tau \quad \text{size } N \times \tau_\tau \quad (U_\tau \gamma_\tau(t), U_p \gamma_p(t)) \quad \text{size } N \times sp,$$

with derivative

$$W_\tau^T \quad \frac{\partial P_\tau^T V_\tau}{\partial p} \quad (U_\tau \gamma_\tau(t), U_p \gamma_p(t)) \quad U_p \quad \text{size } \tau_\tau \times N, \text{ sparse} \quad \text{size } N \times sp.$$

In the applied finite element method a single functional component of $F_n$ only depends on a small constant number $c \in \mathbb{N}$ components of $U_\tau \gamma_\tau(t)$. Thus, the matrix-vector multiplication in the derivative does not really depend on $N$ since the number of entries per row in the Jacobian is at most $c$.

But there is still a dependence on $N$, namely the calculation of $U_\tau \gamma_\tau(t)$. To overcome this dependency we identify the required components of the vector $U_\tau \gamma_\tau(t)$ for the evaluation of $P_\tau^T V_\tau$. This is done by defining selection matrices $Q_{n,n} \in \mathbb{R}^{c \times \tau_\tau}$, $Q_{n,p} \in \mathbb{R}^{c \times sp}$ such that

$$P_\tau^T V_\tau (U_\tau \gamma_\tau(t), U_p \gamma_p(t)) = \hat{F}_n (Q_{n,n} U_\tau \gamma_\tau(t), Q_{n,p} U_p \gamma_p(t)),$$

where $\hat{F}_n$ denotes the functional components of $F_n$ selected by $P_\tau$ restricted to the arguments selected by $Q_{n,n}$ and $Q_{n,p}$.

Supposed that $\tau_\tau \approx s_\tau \ll N$ we obtain a reduced order model which does not depend on $N$ any more.

### 3 Numerical investigation

The discussed finite element method is implemented in C++ based on the finite element library deal.II [11]. The high dimensional DAE is integrated using the DASPK software package [12]. The derivative of the nonlinear functional is hard to compute and thus we calculate the Jacobians by automatic differentiation with the package ADOL-C [13]. The Newton systems which arise from the BDF method are solved with the direct sparse solver SuperLU [14].
A basic test circuit with a single 1-dimensional diode is depicted in Fig. 1. The parameters of the diode are summarized in [5]. The input $v_s(t)$ is chosen to be sinusoidal with amplitude $5\ [V]$. In the sequel the frequency of the voltage source will be considered as a model parameter.

We first validate the reduced model at a fixed reference frequency of $5 \cdot 10^9\ [Hz]$. Fig. 2 shows the development of the relative error between the POD reduced, the POD-DEIM reduced and the unreduced numerical solutions, plotted over the lack of information $\Delta$ of the POD basis functions with respect to the space spanned by the snapshots. The figure shows that the approximation quality of the POD-DEIM reduced model is comparable with the more expensive POD reduced model. The number of POD basis functions $s(\cdot)$ for each variable is chosen such that the indicated approximation quality is reached, i.e. $\Delta := \Delta_{\psi} \simeq \Delta_{J_n} \simeq \Delta_{J_p} \simeq \Delta_{\psi} \simeq \Delta_{\psi} \simeq \Delta_{\psi} \simeq \Delta_{\psi} \simeq \Delta_{\psi}$. The numbers $\tau(\cdot)$ of POD-DEIM basis functions are chosen likewise.

In Fig. 3 the simulation times are plotted versus the lack of information $\Delta$. The POD reduced order model does not reduce the simulation times significantly for the chosen parameters. The reason for this is the dependency on the number of variables of the unreduced system. Here, the unreduced system contains 1000 finite elements which yields 12012 unknowns. The POD-DEIM reduced order model behaves very well and leads to a reduction in simulation time of about 90% without reducing the accuracy of the reduced model. However, we have to report a minor drawback; not all tested reduced models converge for large $\Delta(s) \geq 3 \cdot 10^{-5}$. This is indicated in the figures by missing squares.
In Fig. 4 we plot the corresponding total number of required POD basis functions. It can be seen that with the number of POD basis functions increasing linearly, the lack of information tends to zero exponentially. Furthermore, the number of DEIM interpolation indices behaves in the same way.

In Fig. 5 we investigate the dependence of the reduced models on the number of finite elements $N$. One sees that the simulation times of the unreduced model depend linearly on $N$. The POD reduced order model still depends on $N$ linearly with a smaller constant. The dependence on $N$ of our DEIM-POD implementation is negligible.

Finally, we in Fig. 6 analyze the behaviour of the models with respect to parameter changes. We consider the frequency of the sinusoidal input voltage as model parameter. The reduced order models are created based on snapshots gathered in a full simulation at a frequency of $5 \cdot 10^9 [\text{Hz}]$. We see that the POD model and the POD-DEIM model behave very similar. The adaptive refinement of the reduced model is discussed in [5].

Summarizing all numerical results we conclude that the significantly faster POD-DEIM reduction method yields a reduced order model with the same qualitative behaviour as the reduced model obtained by classical POD-MOR.

Acknowledgements The work reported in this paper was supported by the German Federal Ministry of Education and Research (BMBF), grant no. 03HIPAE5. Responsibility for the contents of this publication rests with the authors.
Fig. 6 The reduced models are compared with the unreduced model at various input frequencies.

References